

Robust Nonlinear Control Based on Artificial Intelligence for Electric Vehicles Under Several Constraints

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ABSTRACT

In this paper, we propose a neural network algorithm to eliminate uncertainties caused by dynamic compensators used to linearize permanent magnet synchronous motors for electric vehicle traction. To do this, we propose a speed controller based on an artificial neural network algorithm to approximate the dynamics and correlate the uncertain environmental parameters. We first estimate these uncertainties and use them as inputs to the ANN. We then find an adaptation law to eliminate the uncertainties caused by the compensators. The effectiveness and success of the proposed approach compared to classical controllers in different scenarios of electric vehicle traction are demonstrated by simulations of the adaptive ANN on Matlab/Simulink.

Keywords: PMSM, PI controller, Robust, vector control, fuzzy logic, artificial neuron network, electric desired speed

Introduction

Numerous scientists have proven that vehicles powered by fuel-burning internal combustion engines are the cause of numerous respiratory and carcinogenic diseases, and also air pollution through emissions of nitrogen oxides and carbon dioxide. Electric vehicles, on the other hand, disperse no pollution at all [1,2]. Because they have no exhaust, there is no combustion. But its model is very complex due to its many different parts, such as vehicle dynamics, transmission, and electrical machines [3].

One of the parts of the electric vehicle model is the permanent magnet synchronous motor (*PMSM*) [4], which represents the best option for an electric vehicle drive system given these advantages less maintenance and the simplicity of the mathematical model that will be detailed and discussed in this article [5,6,7]. Nevertheless, the problem of regulating its speed has become a subject of interest for many scientists, as have the limitations of conventional regulators in the face of parametric changes in the permanent magnet synchronous machine model [8].

In this controversy several works have emerged to unravel this type of problem, among these works we can distinguish the nonlinear control method (*CNL*) [10]. Nonlinear control theory deals with nonlinear systems, time-varying or both, and covers a broader class of systems that do not obey the superposition principle. This applies to real-world systems because all real-world control systems are nonlinear and are often governed by nonlinear differential equations. Nonlinear control methods have found applications in various fields such as process control, biomedical engineering, robotics, aircraft

and spacecraft control, electrical machines, electric vehicles, *ABS* system.

The control theory discussed has seen notable advancements in the past twenty years, particularly with the integration of the state feedback linearization technique incorporating input-output decoupling, rooted in field orientation control (*FOC*). The conventional proportional-integral (*PI*) controller is widely employed in speed regulation algorithms and path tracking for permanent magnet synchronous motors (*PMSM*) owing to its straightforwardness and practicality in implementation.

Nevertheless, the conventional *PI* controller is susceptible to variations in parameters and struggles to address issues like overshooting and handling speed disturbances efficiently. Conversely, *fuzzy control*, while not mandating a precise mathematical model, exhibits robustness. It heavily depends on expert knowledge and linguistic formalism, potentially resulting in steady-state inaccuracies. Moreover, predictive control and active disturbance rejection control can enhance the system's dynamic performance, yet their algorithms are intricate and challenging to implement. Traditional *PI* controllers are sensitive to parameter changes [11,12], making them unable to quickly resolve overshoots and disturbances [13]. *Fuzzy control*, on the other hand, is robust and does not require a precise mathematical model [14,15]. However, it relies heavily on expert knowledge and linguistic formalism, which can lead to inaccuracies in steady state. Predictive control and active control by disturbance rejection can improve dynamic system performance, but their algorithms are complex and difficult to implement quickly. nonlinear control methods, such as *fuzzy logic* strategy, have been proposed to solve these problems. *fuzzy logic* allows humans to reason by providing an inference structure, and fuzzy logic controllers are simple to conceptualize, consisting of an input stage, a processing stage, and an output stage [16,17]. *fuzzy logic* has been applied to various fields, including longitudinal autopilot attitude control, precision stabilized platforms, and speed tracking systems [18,19].

The second stage after creating the dynamic model is to model the internal components of each subsystem, which will give us a rough idea of the type of control strategy to be used [20,21].

Modeling Of PMSM

A. Mathematical model of PMSM:

Taking into account the magnetic circuit's non-saturation state and the sinusoidal distributed magneto motive force (*MMF*) produced by the stator windings, the dynamic model of a Permanent Magnet Synchronous Motor (*PMSM*) in a rotor reference frame can be represented by the following equation. [9,38]:

$$[V_{abc}] = [R \cdot i_{abs}] + \frac{d[\varphi_{abc}]}{dt} \tag{1}$$

Where:

$$[V_{abc}] = \begin{bmatrix} V_a \\ V_b \\ V_c \end{bmatrix} \quad ; \quad [i_{abs}] = \begin{bmatrix} i_a \\ i_b \\ i_c \end{bmatrix} \tag{2}$$

$$[R] = \begin{bmatrix} R & 0 & 0 \\ 0 & R & 0 \\ 0 & 0 & R \end{bmatrix} \quad ; \quad [\varphi_{abc}] = \begin{bmatrix} \varphi_a \\ \varphi_b \\ \varphi_c \end{bmatrix} \tag{3}$$

With $V_{abc}, i_{abs}, \varphi_{abc}$ representing the stator phases 'voltages the stator phases 'currents and the total flux produced by the stator currents. R indicates the resistance of a stator phase.

B. Simplification hypothesis:

Throughout the calculation of the *PMSM* mathematical model in the *d-q* frame, the following assumptions are made [23,24]:

- The absence of saturation in the magnetic circuit.
- The sinusoidal distribution of the *M.M.F* created by the stator windings.
- Hysteresis is negligible with eddy currents and skin effect.
- The notching effect is negligible. The resistance of the windings does not vary with temperature.

Total fluxes are expressed by [24]:

$$[\varphi_{abc}] = [L] \cdot [i_{abs}] + [\varphi'_{abc}] \tag{4}$$

$$[L] = \begin{bmatrix} L_{SS} & M_s & M_s \\ M_s & L_{SS} & M_s \\ M_s & M_s & L_{SS} \end{bmatrix} \text{With:} \tag{5}$$

$$[V_{abc}] = [R] \cdot [i_{abs}] + L \frac{d[i_{abs}]}{dt} + \varphi'_{abc} L_{SS} \text{ and } M_s \text{ representing the self-inductance and the mutual inductance between stator windings. } \varphi'_{abc} \text{ is the rotor flux seen by the stator winding It represents the amplitudes of the voltages induced in the stator phases without load Substituting (4) in (1) :} \tag{6}$$

The electromagnetic torque is expressed by [26]:

$$C_{em} = \frac{1}{\omega_r} [e_{abc}]^t \cdot [i_{abs}] \tag{7}$$

where $e_{abc} = \frac{d\varphi_{abc}}{dt}$ Represents the electromotive force generated by the stator phase. ω_r is the speed of the rotor in $[rad/s]$. Note that system (4) leads to correlated and strongly nonlinear equations. To simplify this problem, most studies in the literature prefer to use Park's transformation, which provides dummy variables denoted *d-q* by transformations applied to real variables (voltage, current, and flux) - the components of the Park's equation are denoted as [23]. From physically, this transformation is interpreted as replacing the stationary windings (*a, b, c*) with rotating windings (*d, q*) that rotate with the rotor. This transformation simplifies the dynamic equations of the *AC* motor. The Park transform is defined as follows [24]:

$$[x_{dq0}] = [K_\theta][x_{abc}] \tag{8}$$

Where *x* can be current, voltage or flux and θ is the rotor position. x_{dq} represents the direct and quadrature components of the stator variables (voltage, current, flux and inductance). The transformation matrix K_θ is given by[25]:

$$[K_\theta] = \sqrt{\frac{2}{3}} \begin{bmatrix} \frac{1}{\sqrt{2}} & \cos(\theta) & -\sin(\theta) \\ \frac{1}{\sqrt{2}} & \cos\left(\theta - \frac{2\pi}{3}\right) & -\sin\left(\theta - \frac{2\pi}{3}\right) \\ \frac{1}{\sqrt{2}} & \cos\left(\theta - \frac{4\pi}{3}\right) & -\sin\left(\theta - \frac{4\pi}{3}\right) \end{bmatrix} \tag{9}$$

The inverse matrix:

$$[K_\theta]^{-1} = \begin{bmatrix} \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \\ \cos(\theta) & \cos\left(\theta - \frac{2\pi}{3}\right) & \cos\left(\theta - \frac{4\pi}{3}\right) \\ -\sin(\theta) & -\sin\left(\theta - \frac{2\pi}{3}\right) & -\sin\left(\theta - \frac{4\pi}{3}\right) \end{bmatrix} \quad (10)$$

Applying the transformation (8) to the system (1), we have the electrical equations in the (d - q) reference [21,22]:

$$V_d = R_s \cdot i_d + L_d \frac{di_d}{dt} - \omega \cdot \varphi_q \quad (11)$$

$$V_q = R_s \cdot i_q + L_q \frac{di_q}{dt} + \omega \cdot \varphi_d \quad (12)$$

The flux equation [24]:

$$\varphi_d = L_d \cdot i_d + \varphi_f \quad (13)$$

$$\varphi_q = L_q \cdot i_q \quad (14)$$

φ_f is the flux created by the magnets in the rotor, By replacing (13) and (14) and in V_d, V_q we obtain the following equations:

$$V_d = R_s \cdot i_d + L_d \frac{di_d}{dt} - P \cdot \omega_r \cdot L_q i_q \quad (15)$$

$$V_q = R_s \cdot i_q + L_q \frac{di_q}{dt} - P \cdot \omega_r \cdot L_d i_d + P \cdot \omega_r \cdot \varphi_f \quad (16)$$

With:

$$\omega = P \cdot \omega_r \quad (17)$$

Electromagnetic torque equation [26]:

$$C_{em} = \frac{3}{2} \cdot P \cdot [(L_d + L_q) \cdot i_d \cdot i_q + \varphi_f \cdot i_q] \quad (18)$$

C. Field oriented control:

Utilizing the field-oriented control mechanism with $i_{dref}=0$ [32,33], the expression for electromagnetic torque in to (18) be simplified as follows:

$$\begin{cases} C_{em} = K_e \cdot i_{qref} \\ K_e = \frac{3}{2} \cdot P \cdot \varphi_d = \frac{3}{2} \cdot P \cdot \varphi_f \end{cases} \quad (19)$$

The goal of the control is to create a control law $i_{qref}(t)$ that enables the output (*speed*) to follow the desired reference speed set by the vehicle accelerator pedal. The tracking error $e_{\omega r}(t)$ ($e_{\omega r}(t) \in R$) is defined as:

$$e(t) = \omega_{ref}(t) - \omega_r(t)$$

In the (*d-q*) Park system, the electrical quantities are of the direct current type giving the possibility to make the control similar to the control of direct current machines [27].

The variables i_d and i_q represent the currents along the *d-q* axis, the variables V_d, V_q represent the stator voltages along the *d-q* axis obtained by the Park transformation, C_{em} represents the electromechanical torque of the *PMSM*, C_r represents the resistive torque in our case it is the dynamics of the vehicle, ω_r represents the mechanical speed of rotation, φ_d, φ_q Represents the flux along the *d-q* axis:

R: Stator resistance on the referential (*d-q*).

L_d, L_q : the inductance on the reference frame (*d-q*).

P: number of pole pairs.

f: coefficient of friction.

Vehicle dynamics

The speed of a vehicle can be expressed as a constant tractive force to be provided as a function of the characteristics of the vehicle (Fig.1), such as: the mass M_v , the rolling friction *f*, its coefficient of penetration in the air C_x and, also on the slope of the road α % of a sum total of the equations of the forces exercised on the vehicle. [29]

The traction force required to move the *EV* is given by the sum of the rolling resistance forces added to the acceleration force F_{acc} [30]. As shown in Fig.1, the rolling resistance forces, detailed by the group of equations (21), are:

- The aerodynamic force F_{aero} .
- The force F_{roul} due to the contact of the wheels on the road.
- the gravitational force F_{gx} due to the slope α .

The resistant torque created by the vehicle dynamics is given by the following formula [31]:

$$C_{roul} = F_{trac} \cdot V_{veh} \quad (20)$$

$$\begin{cases} F_{aero} = \rho \cdot \frac{(V_{veh-reel})^2}{2} \cdot C_x \cdot S_f \\ F_{roul} = M_v \cdot g \cdot \cos \alpha \cdot (C_0 + C_1 \cdot V_{veh})^2 \\ F_{gx} = M_v \cdot g \cdot \sin \alpha \\ F_{acc} = M_v \cdot \gamma \end{cases}$$

(21)

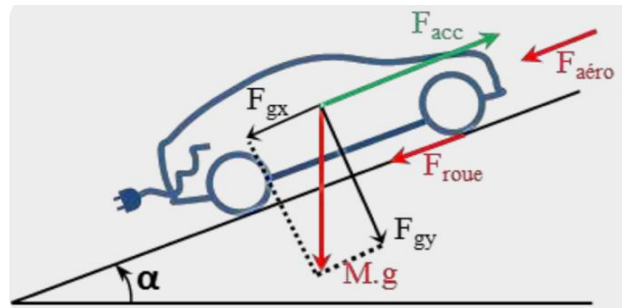


Fig. 1. Forces on a rolling *EV*

Knowing that:

$$V_{veh-re\acute{e}l} = V_{veh} \pm V_{vent}(22)$$

The force of traction is:

$$F_{trac} = F_{acc} - F_{aero} - F_{roul} - F_{gx} \tag{23}$$

Structure of the order

To validate the developed model, tests were performed in the *Matlab/Simulink* environment using the parameters shown in Table 1 and 2. The studied system was subjected to various working conditions. Based on the different mathematical laws of the nonlinear control, the control scheme was developed, which combines the two methods (*PI control* and *Fuzzy logic control*) with its controllers for the variable speed drive of the *PMSM* with a mechanical load representing the vehicle dynamics as shown in Fig.2

This block diagram is decomposed in three essential block a block which represents the *PMSM* with its decoupling, controlled by the vector control, the second block represents the dynamics of vehicle which was translated by a torque resistant compared to the *PMSM*, the third block rests on the part control on the speed of rotation which based on the correction of the error

$$e = e_{\omega_r} = (\omega_{ref} - \omega_r)(24)$$

$$de = \frac{de_{\omega_r}}{dt} = \frac{d\omega_{ref}}{dt} - \frac{d\omega_r}{dt} \tag{25}$$

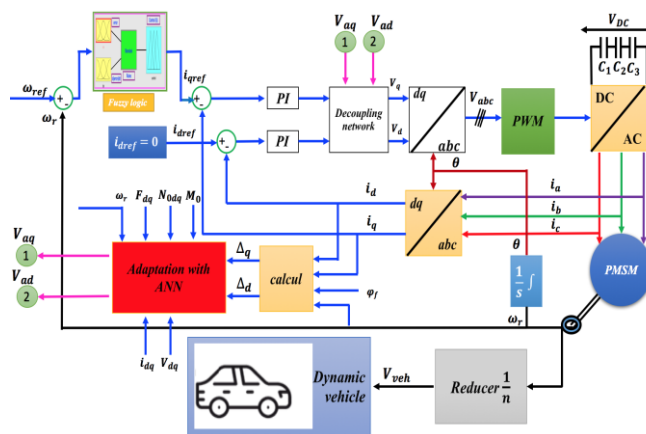


Fig. 2. Block diagram of PMSM with adaptation controller

Equations (24) and (25) represent the inputs of the fuzzy logic controller (fig.4). Considering the progress made in normalization.

D. PI Regulation:

In this traditional approach, the Integral Proportional (PI) controller is utilized to rectify the discrepancy between the desired rotational speed and the actual measured rotation speed [32]. In this Controller, the input to the system is the error with constant gain (K_p) in addition to the integral of the error e with constant gain (K_i) to control the system output w_r as the fig.3. By using the pumping method, we will have the regulator gains as follows: The values of K_{pw} and K_{iw} are respectively 1.735 and 22.5 .By using the decoupling of the vector control, the equation (26) represents the regulation of the currents by the principle of *PI* regulator, for the speed control we will have the equation (27) which gives a reference electromagnetic torque from dynamic rotation speed error

$$V_{dqr} = K_{pdq}(i_{dqr} - i_{dq}) + \frac{1}{K_{idq}} \int (i_{dqr} - i_{dq}) \tag{26}$$

$$C_{em_ref} = K_{pw} \cdot (\omega_{ref} - \omega_r) + \frac{1}{K_{iw}} \int (\omega_{ref} - \omega_r) \tag{27}$$

Equations (26) and (27) represent the mathematical formula calculations under the PI regulation

E. Fuzzy logic regulation:

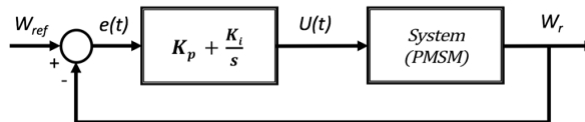


Fig. 3. Functional diagram of a system regulated by the PI regulator

The fuzzy controller employed is of the Mamdani type, structured around a decision-making framework that handles subjective and imprecise rules. The initial stage in developing a fuzzy controller involves selecting its input and output variables, determining the parameters required for the desired outcome, and defining the linguistic ranges of its variables. The system inputs are the error of the angular position **e** and its derivative **de** (equations (24) and (25)). The fuzzy controller is composed:

1. A rule base, which contains the rules describing the expert's conduct.
2. From a decision making logic.
3. A FUZZIFICATION interface, which allows transforming the measured input values into measured values into fuzzy values.
4. From a DEFUZZIFICATION interface to the output, a precise action is determined from the fuzzy output
5. variables descriptions.

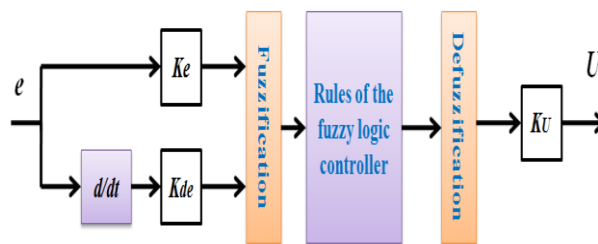


Fig. 4. Functional diagram of a system regulated by the Fuzzy logic controller

Fuzzy logic can deal with situations that are uncertain where the domain knowledge is represented by linguistic variables (SMALL, MEDIUM, LARGE, etc.) with membership values ranging from 0 to 1. Fuzzification, inference, and defuzzification are the three steps of the FLC system.

Our study was initiated by establishing fuzzy sets of input and output variables with membership functions of 3, then 5. Comparing the results, we found that the five-set regulator works better.

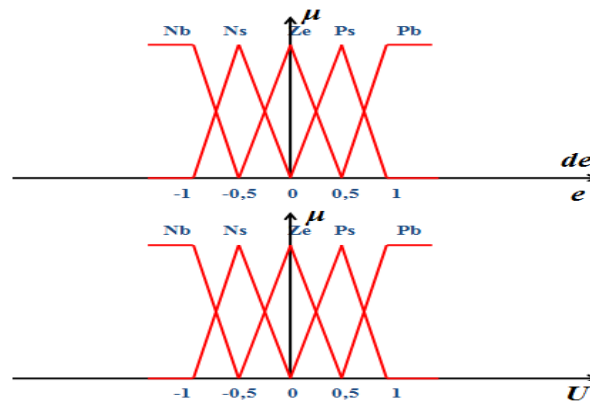


Fig. 5. Membership functions for: input (e , de), and output (U) The fuzzy rules are listed in Table 1

The five fuzzy sets that characterize the variables A Mamdani fuzzy logic controller was created with two inputs and one output, each partitioned into five fuzzy sets: Nb (large negative), Ns (small negative), Ze (zero), Ps (small positive), and Pb (large positive). *Gaussian* and *triangular* membership functions were chosen for the inputs and output variables [33]. The Mamdani controller is commonly employed as a feedback controller, establishing a static relationship between the input conditions and the corresponding output actions. This controller mirrors the continuous decision-making process of humans and enables seamless transition between discrete output values. The antecedent and consequent fuzzy sets in Mamdani systems are typically triangular or Gaussian, with input membership functions overlapping in a manner that ensures the membership values of the rule antecedents always sum to one. This design choice allows for a smooth transition between discrete outputs, capturing the continuous nature of human decision-making processes. Mamdani fuzzy inference systems are well suited to expert systems applications where rules are created from human expert knowledge, such as medical diagnoses. The inference process of a Mamdani system involves combining the output fuzzy sets into a single fuzzy set using the FIS aggregation method, then defuzzification the combined output fuzzy set to calculate a final output value sharp. *Fuzzy-PI* controllers have two inputs and one output. The *Fuzzy-PI* controller in Figure 2 is developed using input membership functions for the error e and the change in error of and output membership function for W_r , the measured velocity for *PMSM*. [32] During the simulation of the system with the fuzzy logic control technique, the toolbox rules are shown in Figure 3 and 4, which characterize the correction of the error (e) and the variation of the error (de) of in the interval $[-1\ 1]$. The normalization gains " K_e " and " K_{de} " for the committed error and the control gain " K_U " for converting the output were added. [33]

The rules of the five-set fuzzy controller is shown in Table 1 [39]:

TABLE I
RULES OF THE FUZZY LOGIC CONTROLLER

de	Nb	Ns	Ze	Ps	Pb
e					
Nb	Nb	Nb	Ns	Ze	Ze
Ns	Nb	Ns	Ze	Ze	Ze
Ze	Ns	Ze	Ze	Ze	Ze
Ps	Ns	Ze	Ze	Ps	Ps
Pb	Ze	Ze	Ps	Pb	Pb

F. Neural Network Controller

The utilized neural network features a single hidden layer consisting of eight neurons, with the activation functions "tansig" and "purelin"[34]. The Levenberg-Marquardt algorithm was employed for learning in order to achieve optimal results [34]. Once the network structure was determined, the optimization of connection weights, also known as the learning process, could commence. The structure of the network significantly impacts the learning process and the quality of control, as the approximation error depends on both the number of neurons in the hidden layer and the information input to the network [35].

Mathematically developing the equations of the machine. We have:

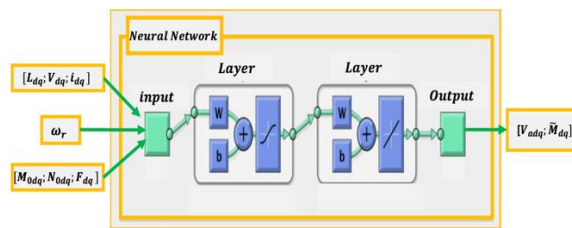


Fig. 6. Type of neural network used

$$\begin{cases} L_d \cdot \frac{di_d}{dt} = V_d - R_s \cdot i_d + P \cdot \omega_r \cdot L_q \cdot i_q \\ L_q \cdot \frac{di_q}{dt} = V_q - R_s \cdot i_q - P \cdot \omega_r \cdot L_d \cdot i_d - P \cdot \omega_r \cdot \varphi_f \end{cases} \quad (28)$$

Equation (28) becomes:

$$\begin{cases} V_d = R_s \cdot i_d + L_d \frac{di_d}{dt} - P \cdot \omega_r \cdot L_q \cdot i_q \\ V_q = R_s \cdot i_q + L_q \frac{di_q}{dt} + P \cdot \omega_r \cdot L_d \cdot i_d + P \cdot \omega_r \cdot \varphi_f \end{cases} \quad (29)$$

According to the equations (29) we obtain:

$$\begin{cases} \frac{di_d}{dt} = \frac{V_d - R_s \cdot i_d}{L_d} + \frac{(P \cdot \omega_r \cdot L_q \cdot i_q)}{L_d} \\ \frac{di_q}{dt} = \frac{V_q - R_s \cdot i_q}{L_q} + \frac{(-P \cdot \omega_r \cdot L_d \cdot i_d - P \cdot \omega_r \cdot \varphi_f)}{L_q} \end{cases} \quad (30)$$

We want to write the system of equation (30) in the following form in (31):

$$\begin{cases} \frac{di_d}{dt} = \frac{U_d}{L_d} + \Delta_d \\ \frac{di_q}{dt} = \frac{U_q}{L_q} + \Delta_q \end{cases} \quad (31)$$

The resulting errors are caused by parametric and driving cycle uncertainties imposed on the electric vehicle (reference speed ω_{ref}) therefore to improve the performance of the permanent magnet synchronous machine(PMSM), two adaptive blocks using artificial neural networks (ANN) were used

to reinforce the system with machine equations for targeted errors Δ_d and Δ_q . Since the controlled system is decoupled into two subsystems, we develop the ANN using two pairs "input /output", namely:

- the d-system: $p=[V_d, i_d]$, and Δ_d as target vector.
- the q-system: $p=[V_q, \omega_r]$, and Δ_q as target vector.

Therefore, the deduced from equations (30) and (31) gives the following expressions for Δ_d and Δ_q

$$\begin{cases} \Delta_d = \frac{(P \cdot \omega_r \cdot L_q \cdot i_q)}{L_d} \\ \Delta_q = \frac{(-P \cdot \omega_r \cdot L_d i_d - P \cdot \omega_r \cdot \varphi_f)}{L_q} \end{cases} \tag{32}$$

G. Control using Neural Networks with Fuzzy Regulators

Once the learning phase has been completed, we turn to the implementation under *Matlab/Simulink* of two neural blocks allowing us to estimate the adaptive terms " V_{ad} " and " V_{aq} " (Fig.7) which will aim to compensate for the targeted disturbance terms Δ_d and Δ_q .

The adaptive terms V_{ad} and V_{aq} gives the possibility to adjust the high uncertainties Δ_d and Δ_q . V_{ad} and V_{aq} are calculated using the following formulas[36]:

$$\begin{cases} V_{ad} = \hat{M}^T \sigma(N_0^T \mu_d) \\ V_{aq} = \hat{M}^T \sigma(N_0^T \mu_q) \end{cases} \tag{33}$$

With:

$$\begin{cases} \mu_d = [V_d \ i_d]^T \\ \mu_q = [V_q \ \omega_r]^T \end{cases} \tag{34}$$

The estimate of M, denoted as \hat{M} , is updated according to the following adaptation law [36,37]:

$$\dot{\hat{M}} = -F_{dq} [2(\sigma(N_0^T \mu_{dq}) \cdot \tilde{v}_{dq} + K_{dq}(\hat{M} - M_0))] \tag{35}$$

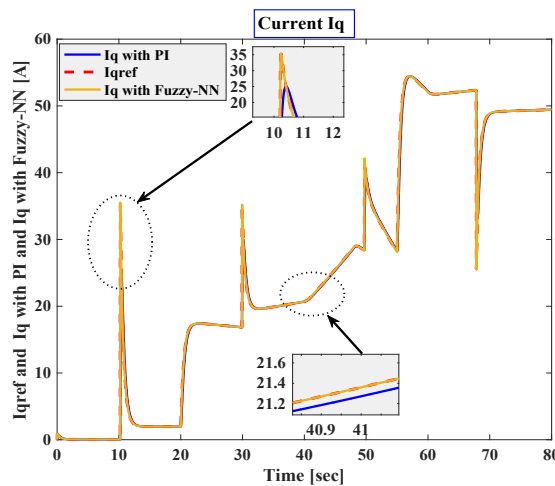


Fig. 10. variation of current I_q

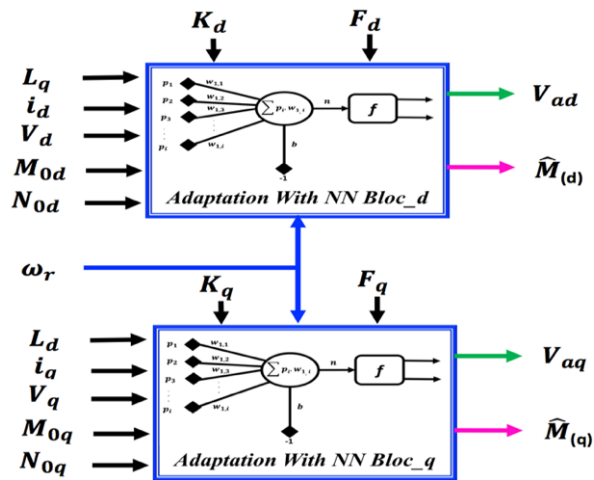


Fig. 7. Adaptive control with neural networks (NN)

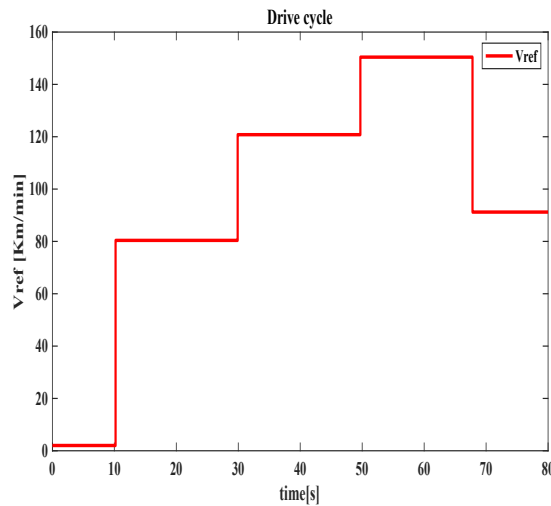


Fig.8. Drive cycle of speed

RESULTS AND DISCUSSION

After subjecting the control system to different working conditions: regulation *PI*, then the second test by the fuzzy neural network control, we obtained the following results:

H. Drive cycle of speed:

The results of the electric vehicle simulation under Matlab/Simulink are illustrated as follows:

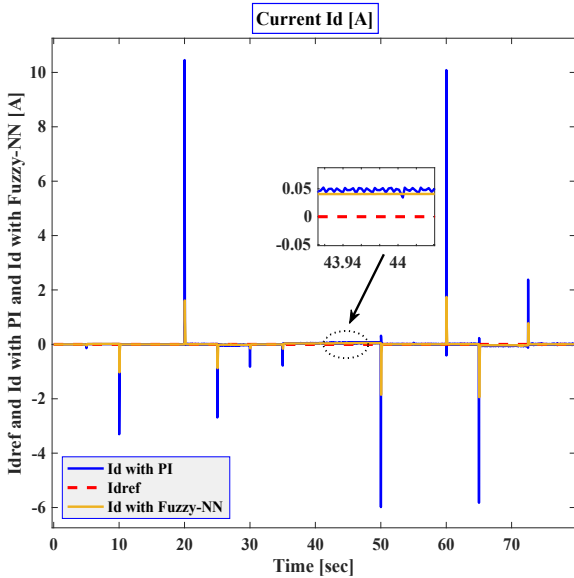


Fig. 9. variation of current I_d

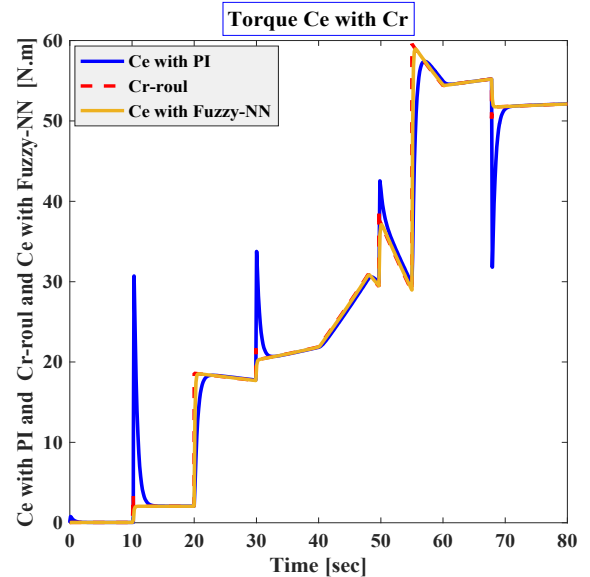


Fig. 11. variation of torque C_{r-roul} and C_e with PI and C_e with $Fuzzy-NN$

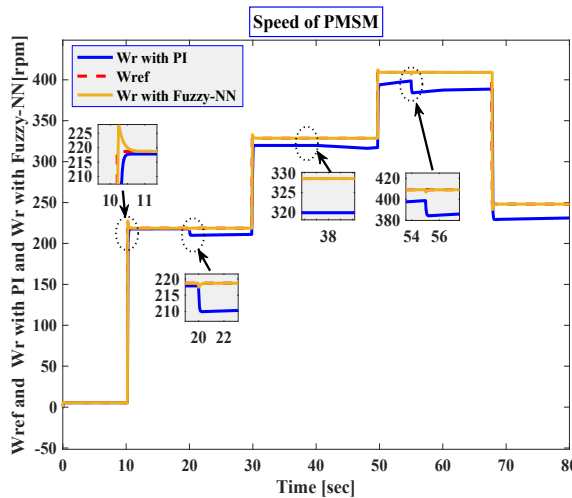


Fig. 12. speed of rotation W_r

The Fig.9. represents the variation of the current of the synchronous motor I_d with permanent magnet as a function of time, according to the two control strategies (PI controller and network regulator of fuzzy neurons), and, we note that the current has peaks author of its reference ($i_{dref}= 0$) which are caused by the variation of the speed and the errors of the modeling. Comparing between the two PI results and with fuzzy reinforced by artificial neural networks, we see that the response obtained by the $Fuzzy-NN$ regulator is closer to the record than that obtained by the PI regulator. The current regulation generates in this case the optimization of the energy consumed by the applied control, a good decoupling of the vector control FOC .

Fig.10. shows the variation in the current I_q of the synchronous permanent magnet motor as a

function of time, according to the two control strategies (PI and fuzzy logic reinforced by the adaptation ANN) we note that the current obtained by the PI regulator (I_q with PI) is almost identical to that obtained by the fuzzy- NN regulator (I_q with Fuzzy- NN) and by a zoom on the range of Matlab, we see a small difference which can be the cause of the comparison between the two commands before the reference. The two strategies are therefore effective for regulating the current, in terms of precision the choice is the $Fuzzy-NN$ command. And by a zoom in the range of Matlab we see a small difference which can be the cause of the comparison between the two commands before the reference. The two strategies are therefore effective for regulating the current, in terms of precision the choice is the $Fuzzy-NN$ command. The two strategies are therefore effective for regulating the current, in terms of precision the choice is the $Fuzzy-NN$ command.

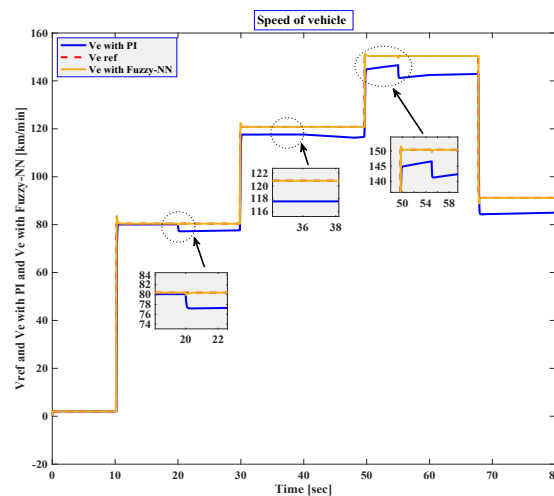


Fig. 13. speed of the vehicle V_e

Fig.11 shows the variation of the electromagnetic torque and the resisting torque created by the dynamics of the vehicle on the electric motor as a function of the time which varies between 0 sec and 80 sec. The two results are good compared to the stress applied to the (C_e engine with PI and C_e with $Fuzzy-NN$) but by direct observation we notice that the torque with C_e with $Fuzzy-NN$ is closer to the set point and follows the resistant couple C_{r-roul} . The torque being varied as a function of time to follow the variation of the resistant torque with small errors caused by the variation of the slope and the variations of the parameters inside the motor against C_e with PI does not follow the resistant couple well, lack of precision.

Fig.12 shows the rotation speed of the synchronous motor as a function of time [0 sec to 80 sec] with the reference speed, by both techniques (W_r with PI and W_r with $Fuzzy-NN$) We observe a good continuation of the instructions by the adaptive fuzzy regulation based on artificial neural networks compared to the PI regulator. On the other hand, in the PI controller, we note the absence of reference tracking caused by the parametric change of the stator resistance R and the stator inductance L . This variation generates the malfunction of the vector control FOC . In this case, precision is a factor that plays an essential role in our system to ensure the proper monitoring and stability of the system. A p% slope at time (20s) of 20° shows the robustness of the control by the zoom of this moment, the same test at time (60s) with an increase of 45°, the zoom at time 60 s indicates the response of the system, so the correct reference follows-The model obtained by the fuzzy regulator reinforced by artificial neural networks. This control is a proof of robustness in the face of parametric change and external uncertainties (applied slope on the trajectory) and in front of the imposed drive cycle.

Fig.13 shows the variation in vehicle speed as a function of time from 0 s to 80 s. This speed is the result of the rotation speed of the $PMSM$ multiplied by the transformation gain in this case where we observe the response obtained by the two strategies (PI and $Fuzzy-NN$), the speed obtained by the PI

(V_e -PI) regulator having deviations with its reference (Zoom at time 36s), which shows the absence of the pursuit, while the *Fuzzy-NN* regulation satisfies this pursuit between the measured value V_e with *Fuzzy-NN*) and the speed reference (V_{ref}) the performance of this vehicle improves in terms of speed in the case of an adaptive fuzz regulator in terms of tension with neural networks

Conclusion

The automaton with fuzzy logic reinforced by an artificial adaptation proves much more robust because the speed of the motor makes it possible to follow much more quickly the reference rotation speed in the case of a change abrupt and in relation to external disturbances, on the other hand the results obtained by the classic regulation (PI regulator) have overshoots concerning the motor torque so the most robust and effective control among these two techniques is the fuzzy control adaptive logic. From the point of view of this work, the control of adaptive fuzzy logic in voltage is effective in the case of changes in parameters of the electric motor, but it lacks sensitivity to engine uncertainty at this stage, the system must improve the target error and external disturbances caused by the environment, the major drawback of the control requires a data and additional information.

Therefore, our system needs adaptive predictive control to improve performance, stability and reference tracking; in the future we will be interested in adaptive predictive control

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